

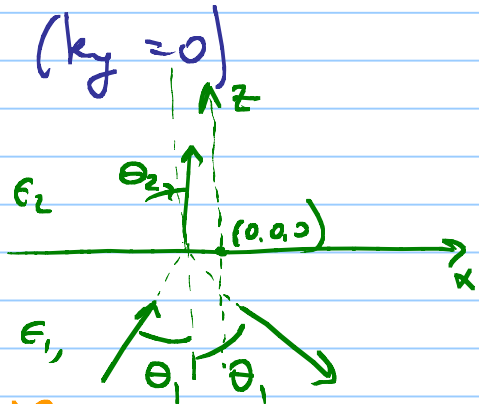
EM II lecture 02 - reflection and transmission

Note Title

12/23/2015

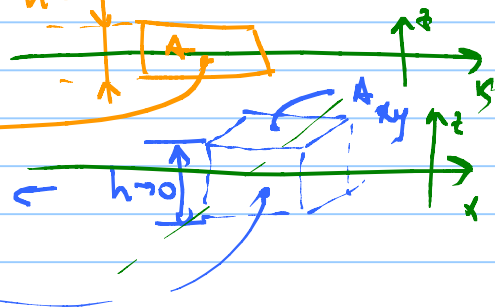
In the previous classes we have shown that plane wave represents a solution of Maxwell equations in a homogeneous material we now consider an interface between two materials. we will assume that the interface is in xy plane and that the light propagates in xz plane ($k_y = 0$)

We again start with Maxwell equations ($\mu = 1$)



$$(2.1a) \left. \begin{aligned} \nabla \times \vec{H} &= \epsilon_0 \vec{\epsilon} \frac{\partial \vec{E}}{\partial t} \\ \nabla \times \vec{E} &= -\mu \frac{\partial \vec{H}}{\partial t} \end{aligned} \right\} \int \vec{A} \rightarrow$$

$$(2.1b) \left. \begin{aligned} \text{div } \vec{B} &= 0 \\ \text{div } \vec{D} &= 0 \end{aligned} \right\} \int d^3 r_a$$



$$\int \nabla \times \vec{H} \cdot d\vec{l} = \int \vec{H} \cdot d\vec{l} = (H_{2z} - H_{1z}) l = \epsilon_0 \int \frac{\partial E}{\partial t} \cdot d\vec{l} = 0$$

$$(2.2a) \Rightarrow \begin{cases} H_{2z} = H_{1z} \\ E_{2z} = E_{1z} \end{cases}$$

$$\int \text{div } \vec{B} \cdot d\vec{a} = \oint \vec{B} \cdot d\vec{a} = (B_{2n} - B_{1n}) A_y = 0$$

$$(2.2b) \Rightarrow \begin{cases} B_{2n} = B_{1n} \\ D_{2n} = D_{1n} \end{cases}$$

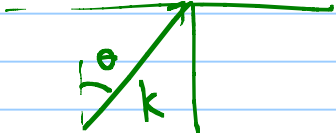
Consider now a situation when a plane wave is incident onto the interface, and exactly one refracted and one reflected plane wave

For a plane wave,

$$(2.3) \quad \vec{E}, \vec{B} = (\vec{E}_0, \vec{B}_0) \cdot e^{i\vec{k} \cdot \vec{r} - i\omega t}$$

Assume that boundary conditions are satisfied @ $\vec{r} = \vec{0}$. Then the p.c. will be satisfied if k_x of all the waves is the same.

Assume that "i", "r", "t" represent incident, reflected, transmitted waves,

$$(2.4) \quad \left. \begin{aligned} k_{ix} &= k_{rx} = k_{tx} \\ \Rightarrow k_1 \sin \theta_i &= k_1 \sin \theta_r = k_2 \sin \theta_t \\ \Rightarrow \sin \theta_i &= \sin \theta_r \Rightarrow \theta_i = \theta_r \\ \Rightarrow k_1 \sin \theta_i &= k_2 \sin \theta_t \stackrel{\text{(isotropic)}}{\Rightarrow} \frac{\omega}{c} n_1 \sin \theta_i = \frac{\omega}{c} n_2 \sin \theta_t \end{aligned} \right\}$$


Note that conservation of $k_x \Leftarrow$ homogeneous interface

(Snell's law)

We now use boundary conditions to calculate transmission & reflection amplitudes.

In isotropic & uniaxial media,

$$\text{TE modes (s): } \vec{E} \parallel \hat{y}; \quad \vec{H} \perp \hat{y}$$

$$\text{TM modes (p): } \vec{E} \perp \hat{y}; \quad \vec{H} \parallel \hat{y} \Rightarrow \text{polarizations don't mix}$$

In general, however they do. We will hence consider general case:

$$(2.5) \quad \vec{E}_i = a_{i1}^+ \vec{E}_{i1}^+ e^{i\vec{k}_{i1}\cdot\vec{r} - i\omega t} + a_{i2}^+ \vec{E}_{i2}^+ e^{i\vec{k}_{i2}\cdot\vec{r} - i\omega t}$$

And similar for E_t, E_r, B_i, B_r, B_t

For uniaxial medium:

$$\vec{E}_{i1}^+ = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}; \quad \vec{E}_{i2}^+ = \begin{bmatrix} k_{z12} \epsilon_{2,1} \\ 0 \\ -k_x \epsilon_{1,1} \end{bmatrix}$$

$$\vec{H}_{i1}^+ = \frac{1}{\mu\omega} \begin{bmatrix} +k_z \\ 0 \\ k_x \end{bmatrix}; \quad \vec{H}_{i2}^+ = \frac{1}{\mu\omega} \begin{bmatrix} \hat{x} & \hat{y} & \hat{z} \\ k_x & 0 & \pm k_z \\ \pm k_z \epsilon_{1,1} & 0 & -k_x \epsilon_{1,1} \end{bmatrix}$$

$$= \frac{1}{\mu\omega} \begin{bmatrix} 0 \\ k_x^2 \epsilon_1 + k_z^2 \epsilon_2 \\ 0 \end{bmatrix} = \frac{\omega \epsilon_1 \epsilon_2}{c^2} \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}$$

Overall the 4 boundary conditions (continuity of $E_{\parallel}, H_{\parallel}$) can be written as:

$$B_1 \quad k_{z12} \epsilon_{2,1} (a_{i2} - a_{r2}) = k_{z22} \epsilon_{2,2} a_{t2}$$

$$B_2 \quad a_{i1} + a_{r1} = a_{t1}$$

$$H_1 \quad -\frac{k_{z11}}{\mu_1 \omega} (a_{i1} - a_{r1}) = \frac{k_{z21}}{\mu_2 \omega} a_{t1}$$

$$H_2 \quad \frac{\omega \epsilon_{1,1} \epsilon_{2,1}}{c^2} (a_{i2} + a_{r,2}) = \frac{\omega}{c^2} \epsilon_{2,1} \epsilon_{2,2} (a_{t,2})$$

$$(2.6) \quad \begin{bmatrix} 0 \\ 1 \\ -\frac{k_{z1}}{\mu_1 \omega} \\ 0 \end{bmatrix} a_{i1}^{(c)} + \begin{bmatrix} k_{z2}^{(c)} \epsilon_2^{(c)} \\ 0 \\ 0 \\ \frac{\omega}{c^2} \epsilon_1^{(c)} \epsilon_2^{(c)} \end{bmatrix} a_{i2}^{(c)} + \begin{bmatrix} 0 \\ 1 \\ \frac{k_{z1}}{\mu_1 \omega} \\ 0 \end{bmatrix} a_{r1}^{(c)} + \begin{bmatrix} -k_{z2}^{(c)} \epsilon_2^{(c)} \\ 0 \\ 0 \\ \frac{\omega}{c^2} \epsilon_1^{(c)} \epsilon_2^{(c)} \end{bmatrix} a_{r2}^{(c)}$$

$$\begin{bmatrix} 0 \\ 1 \\ -\frac{k_{22}^{(2)}}{\mu^{(2)}\omega} \\ 0 \end{bmatrix} Q_1^{(1)} + \begin{bmatrix} k_{22}^{(2)} \epsilon_2^{(2)} \\ 0 \\ 0 \\ \frac{\omega}{c^2} \epsilon_1^{(2)} \epsilon_2^{(2)} \end{bmatrix} Q_2^{(1)}$$

Rearrange (2.6)

$$(2.7) \quad \begin{bmatrix} 0 & -k_{22}^{(1)} \epsilon_2^{(1)} & 0 & -k_{22}^{(2)} \epsilon_2^{(2)} \\ 1 & 0 & 1 & 0 \\ \frac{k_{21}^{(1)}}{\mu^{(1)}\omega} & 0 & \frac{k_{22}^{(2)}}{\mu^{(2)}\omega} & 0 \\ 0 & \frac{\omega}{c^2} \epsilon_1^{(1)} \epsilon_2^{(1)} & 0 & \frac{\omega}{c^2} \epsilon_1^{(2)} \epsilon_2^{(2)} \end{bmatrix} \begin{bmatrix} Q_1^r \\ Q_2^r \\ Q_1^t \\ Q_2^t \end{bmatrix} =$$

$$\begin{bmatrix} 0 & -k_{22}^{(1)} \epsilon_2^{(1)} \\ 1 & 0 \\ \frac{k_{21}^{(1)}}{\mu^{(1)}\omega} & 0 \\ 0 & \frac{\omega}{c^2} \epsilon_1^{(1)} \epsilon_2^{(1)} \end{bmatrix} \begin{bmatrix} Q_1^i \\ Q_2^i \end{bmatrix}$$

M_2

$$(2.8) \Rightarrow \begin{bmatrix} \hat{S} \\ \hat{T}_r \end{bmatrix} = (M_1^{-1} \cdot M_2) \begin{bmatrix} Q_1^r \\ Q_2^r \\ Q_1^t \\ Q_2^t \end{bmatrix} = (M_1^{-1} \cdot M_2) \begin{bmatrix} Q_1^i \\ Q_2^i \end{bmatrix}$$

scat (reflect) matrix

transmission matrix

Matrices \hat{S} and \hat{T}_r solve the problem of

reflection/transmission of a plane wave from the interface that is @ $z=0$.

Consider now a case when not one, but two plane waves enter the interface (with same k_x)

(2.8b) Then,

$$\begin{bmatrix} a_1^r \\ a_2^r \\ a_1^t \\ a_2^t \end{bmatrix} = (\bar{M}_1^{-1} \cdot \bar{M}_2) \begin{bmatrix} a_1^i \\ a_2^i \\ \tilde{a}_1^i \\ \tilde{a}_2^i \end{bmatrix}$$

(2.7b) with

$$\tilde{M}_2 = \begin{bmatrix} 0 & -k_{z2}^{(1)} \epsilon_2^{(1)} & 0 & -k_{z2}^{(2)} \epsilon_2^{(2)} \\ 1 & 0 & 1 & 0 \\ \frac{k_{z1}^{(1)}}{\mu^{(1)} \omega} & 0 & \frac{k_{z1}^{(2)}}{\mu^{(2)} \omega} & 0 \\ 0 & \frac{\omega}{c^2} \epsilon_1^{(1)} \epsilon_2^{(1)} & 0 & \frac{\omega}{c^2} \epsilon_1^{(2)} \epsilon_2^{(2)} \end{bmatrix}$$

Consider now the interface that is @ $z = z_0$. Then B.C. (2.7) are replaced by

$$M_1 \begin{bmatrix} e^{-ik_{z1}^{(1)} z_0} a_1^r \\ e^{-ik_{z2}^{(1)} z_0} a_2^r \\ e^{ik_{z1}^{(2)} z_0} a_1^t \\ e^{ik_{z2}^{(2)} z_0} a_2^t \end{bmatrix} = \tilde{M}_2 \begin{bmatrix} e^{ik_{z1}^{(1)} z_0} a_1^i \\ e^{ik_{z2}^{(1)} z_0} a_2^i \\ e^{-ik_{z1}^{(2)} z_0} \tilde{a}_1^i \\ e^{-ik_{z2}^{(2)} z_0} \tilde{a}_2^i \end{bmatrix}$$

or, introduce a matrix $F =$

$$\begin{bmatrix} e^{ik_{z1}^{(1)} z_0} & 0 & 0 & 0 \\ 0 & e^{ik_{z2}^{(1)} z_0} & 0 & 0 \\ 0 & 0 & e^{-ik_{z1}^{(2)} z_0} & 0 \\ 0 & 0 & 0 & e^{-ik_{z2}^{(2)} z_0} \end{bmatrix}$$

we obtain:

$$M_1 \begin{bmatrix} \hat{T}_1 \\ \hat{R}_1 \end{bmatrix} = M_2 \begin{bmatrix} \hat{T}_2 \\ \hat{R}_2 \end{bmatrix}$$

(2.8c) or,

$$\begin{bmatrix} a_1 \\ a_2 \\ a_1^t \\ a_2^t \end{bmatrix} = \hat{T}_1 M_1^{-1} \tilde{M}_2 \hat{T}_2 \begin{bmatrix} a_2 \\ a_1 \\ a_2^t \\ a_1^t \end{bmatrix}$$

We have developed Scat. matrix formalism that can be used to calculate T/R from multilayer stacks:

- ① At interface calculate the matrix M_1, \tilde{M}_2 and split it as:

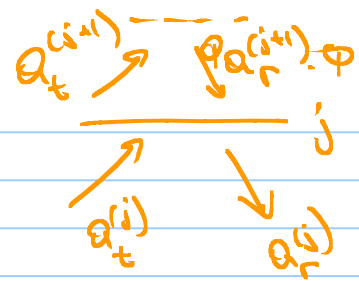
(2.9a) $M_1, \tilde{M}_2 = \begin{bmatrix} \hat{P}_b & \hat{T}_t \\ \hat{T}_b & \hat{P}_t \end{bmatrix}$

- ② Consider "last" interface

(2.9b) $\hat{T}_b^{(n)} = \hat{T}_t^{(n)} \Leftrightarrow \begin{bmatrix} a_t^{(n+1)} \\ a_r^{(n)} \end{bmatrix} = \begin{bmatrix} T_b^{(n)} \\ P_b^{(n)} \end{bmatrix} \begin{bmatrix} a_t^{(n)} \\ a_r^{(n)} \end{bmatrix}$

③ Iterate down:

$$\tilde{a}_i = \hat{\Phi} R_b^{(i+1)} \hat{\Phi} a_t^{(i+1)}$$



(see)

$$\begin{cases} a_t^{(i+1)} = T_b^{(i)} a_t^{(i)} + R_t^{(i)} \hat{\Phi} \tilde{a}_r^{(i+1)} \hat{\Phi} a_r^{(i+1)} \\ a_r^{(i)} = R_b^{(i)} a_t^{(i)} + T_t^{(i)} \hat{\Phi} \tilde{a}_r^{(i+1)} \hat{\Phi} a_r^{(i+1)} \end{cases}$$

$$\begin{cases} \tilde{T}_b^{(i)} = (\hat{I} - R_t^{(i)} \hat{\Phi} \tilde{R}_b^{(i+1)} \hat{\Phi})^{-1} \hat{T}_b^{(i)} \\ \tilde{R}_b^{(i)} = (R_b^{(i)} + T_t^{(i)} \hat{\Phi} \tilde{R}_b^{(i+1)} \hat{\Phi} \tilde{T}_b^{(i)}) \end{cases}$$

While iterating, store $T_b^{(i)}$ & $R_b^{(i)}$ matrices

④ Calculate \vec{a}_t^i, \vec{a}_r^i

Calculate transmittance/reflectance based on Poynting flux calculations!

Alternative formulation PBFs

Note that boundary conditions (2.6) can be written in a different way, Introduce

(2.10)

$$\begin{bmatrix} 0 & k_{22}^{(i)} \epsilon_2^{(i)} & 0 & -k_2^{(i)} \epsilon_2^{(i)} \\ 1 & 0 & 1 & 0 \\ -\frac{k_{21}^{(i)}}{\mu^{(i)} \omega} & 0 & \frac{k_{21}^{(i)}}{\mu^{(i)} \omega} & 0 \\ 0 & \frac{\omega \epsilon_1^{(i)} \epsilon_2^{(i)}}{c^2} & 0 & \frac{\omega}{c^2} \epsilon_1^{(i)} \epsilon_2^{(i)} \end{bmatrix} = \mathcal{N}^{(i)} \begin{bmatrix} E_x \\ E_y \\ H_x \\ H_y \end{bmatrix}$$

$$\hat{F}^{(i)} = \begin{bmatrix} e^{ik_2^{(i)} z_0} & 0 & 0 & 0 \\ 0 & e^{ik_2^{(i)} z_0} & 0 & 0 \\ 0 & 0 & e^{-ik_2^{(i)} z_0} & 0 \\ 0 & 0 & 0 & e^{-ik_2^{(i)} z_0} \end{bmatrix},$$

equ. (2.6) transform to:

$$(2.11) \quad \hat{N}^{(i+1)} \hat{F}^{(i+1)} \begin{bmatrix} \vec{a}_t^{(i+1)} \\ \vec{a}_r^{(i+1)} \end{bmatrix} = \hat{N}^{(i)} \hat{F}^{(i)} \begin{bmatrix} \vec{a}_t^{(i)} \\ \vec{a}_r^{(i)} \end{bmatrix},$$

ready to:

$$(2.12) \quad \begin{bmatrix} \vec{a}_t^{(i+1)} \\ \vec{a}_r^{(i+1)} \end{bmatrix} = \underbrace{\hat{F}^{(i+1)-1} \hat{N}^{(i+1)-1} \hat{N}^{(i)} \hat{F}^{(i)}}_{\hat{T}^{(i+1,i)}} \begin{bmatrix} \vec{a}_t^{(i)} \\ \vec{a}_r^{(i)} \end{bmatrix}$$

Now, the iteration becomes "trivial":

$$(2.12b) \quad \begin{bmatrix} \vec{a}_t^{(N+1)} \\ \vec{a}_r^{(N+1)} \end{bmatrix} = \left[\prod_{j=1}^N \hat{T}^{(j+1,j)} \right] \begin{bmatrix} \vec{a}_t^{(1)} \\ \vec{a}_r^{(1)} \end{bmatrix}$$

$\hat{T}^{(N+1,1)}$

Now, we can go back to solving T/R problem:

$$(2.13) \quad \begin{bmatrix} \vec{a}_t^{(N+1)} \\ 0 \end{bmatrix} = \begin{bmatrix} \hat{T}_{11} & \hat{T}_{12} \\ \hat{T}_{21} & \hat{T}_{22} \end{bmatrix} \begin{bmatrix} \vec{a}_t^{(1)} \\ \vec{a}_r^{(1)} \end{bmatrix}$$

$$(2.13b) \quad \begin{cases} \hat{\tilde{R}} = -\hat{T}_{22}^{-1} \hat{T}_{21} \\ \hat{\tilde{T}} = \hat{T}_{11} + \hat{T}_{12} \hat{\tilde{R}} = \hat{T}_{11} - \hat{T}_{12} \hat{T}_{22}^{-1} \hat{T}_{21} \end{cases}$$

However, this implementation is often numerically unstable

Nevertheless, the T-matrix formalism is beneficial for calculation of

$$(2.14) \quad \begin{bmatrix} \vec{a}_t^{(N+1)} \\ 0 \end{bmatrix} = \hat{T}^{(N+1,1)} \begin{bmatrix} 0 \\ \vec{a}_r^{(1)} \end{bmatrix}$$

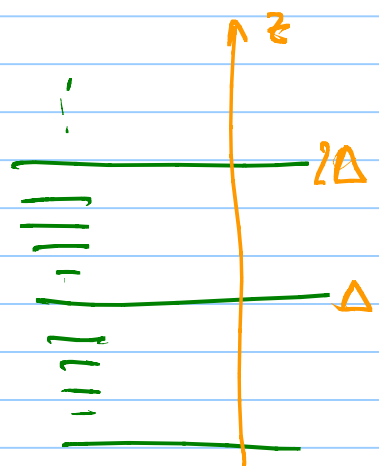
\Rightarrow dispersion can be given by:

$$(2.14b) \quad \hat{T}_{22}^{(N+1,1)} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

\rightarrow photonic crystals:

Consider the periodic layered structure. According to the Bloch hypothesis, the field in such structure should be periodic as well:

$$(E, H)(\Delta) = e^{i q \Delta} (E, H)(0)$$



The field @ a given layer (l) is given by:

$$\underbrace{\begin{bmatrix} \vdots \\ \vdots \\ \vdots \\ \vdots \\ \vdots \end{bmatrix}}_{N^{(l)} \vec{f}^{(l)}} \begin{bmatrix} \vec{a}_t^{(l)} \\ \vec{a}_r^{(l)} \end{bmatrix}$$

⇒ dispersion eq:

$$N^{(p+1)} \vec{f}^{(p+1)} \begin{bmatrix} \vec{a}_t^{(p+1)} \\ \vec{a}_r^{(p+1)} \end{bmatrix} = e^{iq\Delta} N^{(l)} \vec{f}^{(l)} \begin{bmatrix} \vec{a}_t^{(l)} \\ \vec{a}_r^{(l)} \end{bmatrix} \quad \text{P}$$

$$\Rightarrow \left[\hat{N}^{(p+1)} \hat{f}^{(p+1)}(\Delta) \hat{T}^{(p+1,1)} - e^{iq\Delta} N^{(l)} \right] \begin{bmatrix} \vec{a}_t^{(l)} \\ \vec{a}_r^{(l)} \end{bmatrix} = 0$$

same medium

$$(2.15) \quad \hat{N}^{(l)} \left[\hat{f}^{(p+1)}(\Delta) \hat{T}^{(p+1,1)} - e^{iq\Delta} \right] \begin{bmatrix} \vec{a}_t^{(l)} \\ \vec{a}_r^{(l)} \end{bmatrix} = 0$$

eigenvalue-like problem.

dispersion eq:

$$(2.15b) \quad \det \left[\hat{f}^{(p+1)}(\Delta) \hat{T}^{(p+1,1)} - e^{iq\Delta} \hat{T} \right] = 0$$

in. both (2.14) & (2.15) disp. eq. gives $k_x(\omega)$ $[q(\omega, k_x)]$; while \vec{a} give field distribution